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Upscaled engineered functional microfibrillated cellulose flat sheet membranes for removing charged water pollutants

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ABSTRACT

Polymeric composite membranes have shown great potential in removing pollutants from water. A significant limitation of polymeric membranes is the centimeter-sized dimensions, which limit their application at the pilot or industrial scales. In this study, flat sheet functional membranes of microfibrillated cellulose (MFC) with mixed and layered architectures are produced using the up-scaled Dynamic Sheet Former (Formette) in a fully water-based-system, and their potential for the removal of charged impurities from the aqueous medium is evaluated. The processing of composite membranes is unique in terms of size (1m × 20 cm), assembled MFC architectures, tunable porosity, functional groups densities, and free-standing at high water pressure. It is shown that the MFC assembly has a direct influence on the pollutant removal efficiency, and again the layered architecture turns out to be a more efficient scavenger of the charged pollutants due to the combined actions of electrostatic interactions, hydrogen bonding, and size exclusion. Experiments are supported by reactive molecular dynamics simulations that provide possible realistic scenarios at the atomic/molecular scale. All the data confirm the scalability and tunability of the MFC-based water cleaning membranes, which show high adsorption capacity, flexibility, hydrolytic stability, and mechanical robustness.

Keywords: Microfibrillated cellulose, Composite membranes, Metal ions removal, Functional adsorbents, MFC architectures, Computational chemistry

43 SYNOPSIS

44 Results of this article could be easily implemented for removing charged pollutants
45 from water for an effective, sustainable water filter development.

47 INTRODUCTION

48 Among the different types of dangerous substances that are released in the
49 environment, a considerable amount consists of charged metal ions and dyes, which
50 usually come from industrial plants belonging to sectors such as mining, dyeing,
51 electroplating, electrolysis, paper and pulp production, tanning, photography,
52 metallurgy.^{1,2} Conventional methods, such as chemical precipitation, filtration, ion
53 exchange, electrochemical treatment, membrane technologies, adsorption on activated
54 carbon, evaporation, etc., employed for the elimination of these pollutants from the
55 industrial effluents^{3,4} are inefficient, impractical, and insufficient to obtain substantial
56 results. The removal of metal ions by chemical precipitation or electrochemical
57 treatment is ineffective when the ions concentration is between 1-100 mg/L.⁵, and the
58 introduction of new undesirable chemicals (i.e. acids and bases for pH adjustment,
59 flocculating chemicals, coagulants etc.) in the treated water is inevitable. Other
60 conventional approaches like ion exchange, membrane technologies, activated carbon
61 adsorption, or evaporation are costly primarily because of the large energy
62 consumption.^{6,7}

63 Nanocellulose, prepared through a top-down approach from wood biomass, and in
64 particular, MFC, has shown high scavenging potential and thus been tuned for this
65 purpose.⁸⁻¹³ The MFC adsorption capacity and its capability to form stable networks
66 when dried make it an excellent candidate for flat sheet composite membrane (FSCM)
67 processing. As demonstrated in¹⁴ MFC could be a useful, functional, and robust bio-
68 based material in the field of water purification.

69 We are active in the production and application of sustainable bio-based membranes
70 for water purification and focuses on comprehensive multi-disciplinary/scale
71 investigations to understand the process-property-functional correlation and explore
72 the assembly of these small particles within the produced dimensional
73 architecture.^{2,15-17}

74 Another big challenge is the up-scaling of the functional composite membranes
75 without compromising the water flux, selectively, mechanical stability, pore-size
76 distribution. To gain all these properties, Dynamic Sheet Former (Formette) was used
77 for the production of MFC FSCMs at pilot/industrial scale.

78 Thus, his study focuses on (a) the production of FSCM as a prototype for an industrial
79 scale water decentralization system, and (b) the assessment of the MFC assembled
80 architecture (hybrid and layered) relative to the networking potential and the
81 properties of the FSCM. The arrangement and self-assembly of MFC within (hybrid)
82 and on (layered) long fibers networks have been exploited using sophisticated
83 advanced techniques including atomistic molecular dynamics simulations based on a
84 reactive force field (RMD). The potential use of the produced architectures as free-
85 standing membranes for the separation of charged pollutants (metal ions and dyes) in
86 aqueous media is demonstrated. All these aspects are fundamental in the field of

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3 87 affinity membranes as next-generation bio-based membranes for water
4 88 decentralization. The successful results indicate that the synergistic combination of all
5 89 the experimental techniques and computational modeling can be used effectively for a
6 90 thoughtful design of composite membranes with tuned separation capacity of charged
7 91 impurities.
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11 93 **MATERIALS AND METHODS**

12 94 High-grade MFC (Exilva P 01-V) was purchased from Borregaard AB (Sarpsborg,
13 95 Norway). The pulp was supplied by MetsäBoard AB (Husum, Sweden). Dyes
14 96 (Irgalite Blue RL (IB RL) and Irgalite Violet H (IV H)) were purchased from BASF
15 97 Dispersions and Pigments, Germany, and industrial effluent contaminated with metal
16 98 ions were collected from a cellulose production mill (paper and pulp industry) located
17 99 in Sweden. All chemicals were in analytical grade and used without any further
20 100 purifications.
21

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23 102 **Production of FSCM.**

24 103 A complete water-based instrument,¹⁴ Dynamic Sheet Former (Formette) was used for
25 104 the production of MFC assembled flat sheet membranes, as mentioned in **Figure 1**.
26 105 The 1:1 ratio of disintegrated (°SR value 13.6) long pine fibers (0.5 wt%) and MFC
27 106 (0.5 wt%) is taken in the machine chest with continuous stirring and then pumped
28 107 into a perforated cylinder (24×22 cm) through the nozzle (μm pore size). Hybrid
29 108 suspension of long pine fibers and MFC was sprayed on wire mesh having 2000 cm²
30 109 of surface area (20×100 cm). The drainage of the hybrid suspension was performed
31 110 during the spinning of the perforated cylinder at a speed of 3000 rpm for 5 min.
32 111 Semisolid flat sheet hybrid membrane was taken out carefully and dried further using
33 112 a cylindrical dryer at a pressure of 100 kN at 90 °C for 2 min in a continuous mode
34 113 having cylinder speed of 1 m/min. Likewise, for the production of the layered
35 114 structure, first, long pine fibers (0.5 wt%) were sprayed on a wire mesh (base layer),
36 115 and then the pristine MFC (0.5 wt%) was sprayed on the created base layer (**Figure**
37 116 **1**).
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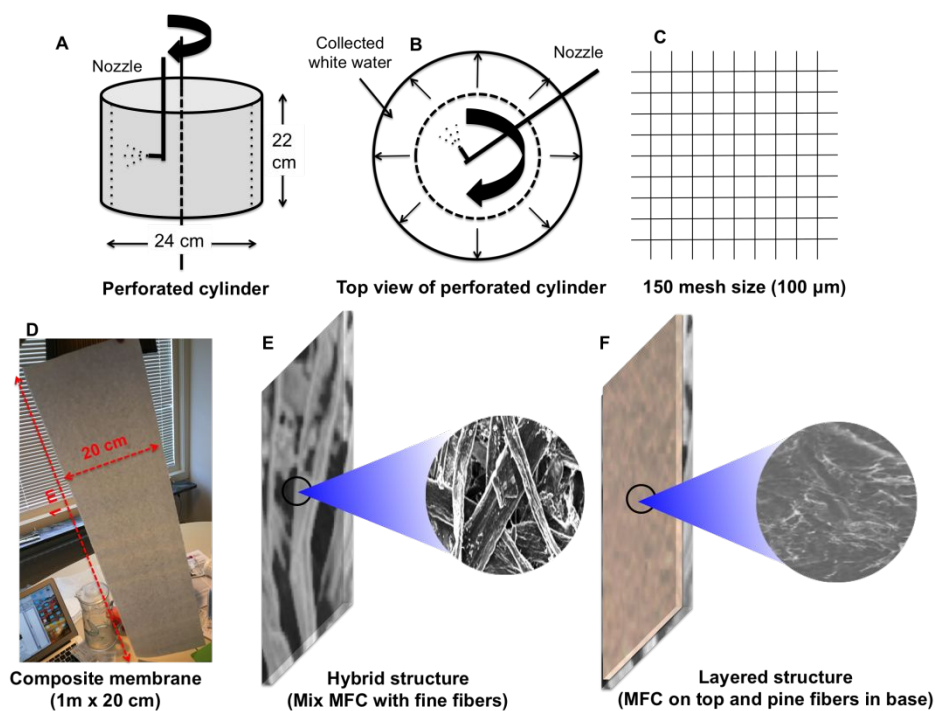


Figure 1. Diagrammatic representation of perforated cylinder (A) of dynamic sheet former used for the production of flat sheet membranes. Nozzle (B) used to spray the MFC and long pine fibers on wire mesh having 100 μm pore diameter (C). Spinning of the cylinder at 3000 rpm responsible for the drainage of water. Two types of self-assembled MFC architecture, hybrid (E) and layered (F) were produced, and fabricated MFC assembled membranes using dynamic sheet former is shown in (D).

CHARACTERIZATION

Mutek SZP 06, MUTEK was used for measuring the surface ζ -potential of the suspensions. Optical morphology of mix suspension (MFC and pine fibers) was obtained using Olympus Polarizing Microscopes (CX31-P). Nano/micro morphology of the composites membranes was captured using low-resolution Scanning Electron Microscope (SEM), JEOL, JSM-6010LV, (Japan). See **SI for details**. The pore-size distribution within composite membranes was measured using N_2 adsorption technique (BET) and Hg-porosimeter (AutoPore IV Micromeritics Instrument Corporation, USA). Porosity was further calculated manually with equation **S1**. Surface wettability tests were carried out using the sessile drop technique at room temperature. Mechanical properties of FSCM were measured with a tensile tester (Lorentzen & Wettre, ABB, Sweden) (**SI**). The water flux through the FSCM was measured using a Convergence Clean Water Flux (CWF) pilot system in continuous mode, at variable pressure, and given temperature (**Figure S2**).

REMOVAL OF CHARGED POLLUTANTS

Dyes. The Irgalite Blue RL and Irgalite Violet H dyes were selected to check the removal capacity of the produced FSCM. The combination of experiment and theory was used to explain possible behaviors of the dyes inside the filtration membranes

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3 147 focusing on representative three-dimensional structures that were downloaded from
4 148 the Cambridge Structural Database (IDs: CUPOCY10 and CEXNIC).^{18,19} These were
5 149 optimized at the quantum chemistry (QC) M06-2X/6-311G(d,p) level of theory in the
6 150 gas phase using the Gaussian09 package (revision A02-)²⁰, and the final geometries
7 151 were employed to estimate two relevant parameters that regulate the motion and
8 152 morphology of the dyes, namely hydrated radius and radius of gyration. The hydrated
9 153 radius was determined using the method proposed by Akbari and co-workers²¹ by
10 154 generating the solvent-accessible surface area (SASA) of each molecule with VMD²²
11 155 (spherical probe with a radius of 1.4 Å) and then calculating the equivalent spherical
12 156 radius. Taking as reference data some of the values reported in **Table S1** of the SI of
13 157 Akbari et al.²¹ we used the correlation between the spherical and hydrated radii to
14 158 estimate the unknown hydrated radius of the two dyes (**Table S1, Figure S3**). Some
15 159 characteristics of the dyes are reported in **Table S2** and **Figure 5C**.
16 160

17 161 **Metal ions.** The industrial effluent collected from the pulp-producing industry, which
18 162 contained various metal ions, was used for the removal study in cross-flow/dynamic
19 163 mode. The effluent was first filtered with a Whatman filter paper 1 (cat. no. 1001090)
20 164 to remove the bio-sludge, and then the filtrate was employed for the separation study.
21 165 The metal ions present in the industrial effluent were Fe²⁺/Fe³⁺, Mg²⁺, Cd²⁺, Co²⁺,
22 166 Cr³⁺ and Mn²⁺ (**Figure 5A**). See details in SI. The measurement of dye and ions
23 167 removal was calculated through Inductive Couple Plasma Atomic Emission
24 168 Spectroscopy (ICP-OES) and UV-visible spectrophotometer(**equation S2**).
25 169

26 170 COMPUTATIONAL MOLECULAR MODELING

27 171
28 172 **Model Building.** Two different models were used to simulate adsorption and
29 173 solvation of the carboxylated layered and hybrid membranes. The first one²³⁻²⁶
30 174 consisted of sixteen aligned glucosyl chains, arranged as a parallelepiped rod with all
31 175 the facets functionalized with carboxyl groups according to the experimental
32 176 indications. The second one (hybrid model) was prepared by placing three fibers, one
33 177 on top of the other (in the Z-direction) rotated by 60 degrees, in a simulation box
34 178 where the initial size was 83.5×89.5×87.5 Å³. (**Figure S4**, See details in SI).
35 179

36 180 **Molecular Dynamics (MD) Simulations.** The production MD simulations were
37 181 performed in the NVT ensemble, and the system configurations were collected every
38 182 0.1 ps. Temperature and pressure were regulated through the Berendsen's thermostat
39 183 and barostat with relaxation constants of 0.1 ps. The time step was set to 0.2 fs. The
40 184 statistical analysis of the sampled data was carried out on the last three hundred
41 185 configurations of the dynamics, considering atom-atom radial distribution functions
42 186 (RDFs) and the percentage of surrounding species (in a 3.5 Å range). A possible
43 187 arrangement of the membrane pores, pockets, tunnels,^{28,29} positions of metal ions and
44 188 solvent molecules was obtained examining the final configurations. This suggested
45 189 possible adsorption trends in the two different architectures (**SI**).
46 190

191 **RESULTS AND DISCUSSIONS**

192

193 **Processing.** A complete water-based system, Dynamic Sheet Former (**Figure 1**), was
 194 used to produce the composite membranes.^{2,14} The 150 wires mesh (100 μm pore
 195 diameter) perforated cylinder was not a clever approach for retention of 5-25 nm
 196 MFC, therefore, pine fibers (22-50 μm in diameter, 0.5 - 1.94 mm range in length and
 197 having surface ζ -potential of -11 ± 24 mV) were introduced to obtain a stable three-
 198 dimensional network *via* hydrophobic/hydrophilic interactions. The loss of MFC
 199 during the fabrication of all the FSCM is shown in **Table 1**.

200

201 **Physical properties.** The thickness of dried reference, hybrid and layered membranes
 202 was 119, 94 and 97 μm , respectively, measured as mentioned in ISO 534. Both
 203 composite membranes have lower thicknesses compared to the reference. Densities at
 204 50% relative humidity varied in the range of 550-702 kg/m^3 , depending on the
 205 composition and preparation conditions. Assuming that the density of MFC was 1500
 206 kg/m^3 , the increased material density, compared with the 100% pine fiber reference
 207 membranes (550 kg/m^3), was related to the addition of MFC (**Table 1**). A high
 208 density of hybrid composite membranes (702 kg/m^3) was recorded even after the loss
 209 of 10.7 % MFC during processing, which could be explained by the decrease in
 210 porosity due to the packing of MFC in the pine fiber network. The obtained results
 211 were further supported by porosity calculation (**Table 1**).¹⁰

212 During the production of layered FSCM, the infusion of the MFC into the base layer
 213 (high load during drying, 100 kN) was observed (≈ 50 to 60 μm), thus, only the
 214 remaining 47 μm was represented by an open loose long pine fibers network, which
 215 might be responsible for the high porosity compared to the hybrid assembled MFC
 216 structure.^{11,30} Hence, the studied up-scaled composite membranes are unique in the
 217 ways of their assembled MFC architectures, which could only and easily be achieved
 218 during processing on dynamic sheet former in a controlled manner. The assembly of
 219 MFC influences the final properties of the composite membranes and the removal of
 220 metal ions as discussed later.

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Table 1: Physical properties of the produced flat sheet membranes.

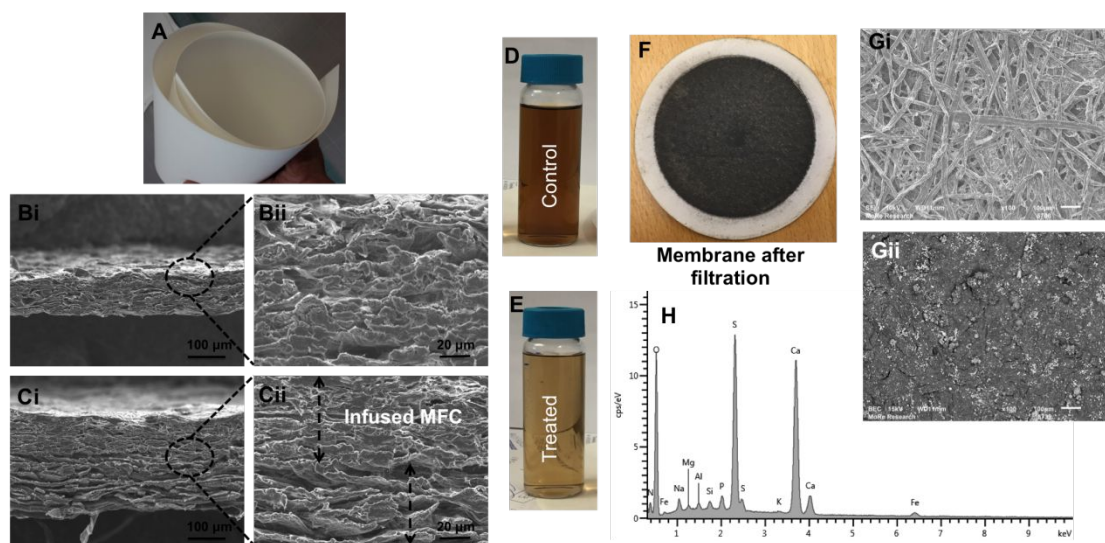
Structures and their compositions	Grammage (g/m^2)		MFC loss (%)	Thickness (μm)	Porosity (%)	Density (kg/m^3)
	Targeted	Obtained				
Ref. structure (100%) PF	65	65	NA	119	48	550
100% PF in bottom and 100% MFC on top), 1 wt%	65 (55 BL and 10 TL)	65	0.00	97	32	616
Hybrid structure (1:1, PF and MFC), 1 wt%	65	58	10.7	94	29	702

223 PF = pine fibers, BL = base layer, TL = top layer, NA = not applicable

224

225 **Morphological studies.** The polarized micrographs of MFC shown in **Figure S1**,
 226 indicate that the fibers have nanometer/micrometer lengths and diameters of a few
 227 nanometers.¹⁰⁻¹³

228 **Figure 2A** shows a the produced FSCM. Cross-section of the flat sheet hybrid
 229 structure at low magnification (**Figure 2bi**), presented a tight network. In parallel,
 230 impregnation of the MFC within the porous dimensional network of pine fibers was
 231 undertaken to ensure that the surface functionality of MFC was readily accessible.¹⁷
 232 In a layered morphology (**Figure 2cii**), a top dense layer and bottom open structure
 233 were observed. The image indicates that the 100kN pressure applied during the drying
 234 of the layered flat sheet structure facilitated the infusion of the top layer into the open
 235 pine base network. Only 10g/m² grammage was targeted for the production of the top
 236 layer, which might not be enough for the production of dual-layered morphologies,
 237 but it could be achieved when low pressure (60 kN), and 1 wt% of cellulosic
 238 nanofibers was used in the fabrication process.¹⁶ The processed membranes using
 239 pilot-scale dynamic sheet former could have some unique morphological
 240 characteristics like the alignment of fibers towards the spin direction, which could not
 241 be achieved using the lab base vacuum-filtration approach. We have also noted that
 242 the water content (moisture) during the processing of membranes could also be
 243 controlled easily during spinning.
 244



245 **Figure 2:** Visual expression (A) and SEM analysis of produced flat sheet membranes. Hybrid flat sheet
 246 membranes in low (Bi) and high (Bii) resolution are shown. Cross- morphology of layered FSCM (Ci
 247 and Cii). For detailed morphology, see supplementary **Figure S5**. Furthermore, the removal experiment
 248 of metal ions in cross-flow mode is shown. (D) and (E) represent the untreated and treated industrial
 249 effluent, respectively. A flat sheet membrane after industrial effluent filtration is shown in (F). SEM
 250 images of used membranes before (Gi) and after (Gii) effluent filtration and finally EDS spectrum of
 251 attached Mg²⁺ ions on the surface of used flat sheet composite membranes (H).
 252
 253

254 **Mechanical performance.** Mechanical properties of the produced membranes were
 255 analyzed in two directions (**Table 2**). We were expecting the alignment of fibers
 256 towards the spin direction (SD). The tensile strength of the reference sample in SD

257 was 21.2 MPa, but ≈ 1.2 fold decrease in strength was calculated in the cross direction
 258 (CD), and a similar trend was noticed for both FSCM (**Table 2**).^{11,31}
 259 Here, membrane drying was performed in continuous mode on a moving cylinder,
 260 which gives a uniform heating effect for the formation of hydrogen bonds and
 261 mechanical stability to the membranes. The high surface area of MFCs increases the
 262 fiber-fiber interaction giving a highly consolidated structure with high tensile strength
 263 and toughness compared to the reference membranes.³²⁻³⁴ The mechanical properties
 264 of the composite membranes were also recorded in wet conditions. The results
 265 followed the same trends as the dry composite membranes, but lower values were
 266 reported.^{15,16}

267
 268 **Table 2:** Mechanical properties of produced membranes in dry and wet conditions

Structures	Tensile strength (MPa)		Strain at break (%)		E-modulus (MPa)		
	SD	CD	SD	CD	SD	CD	
	Dry	Reference (PF)	21.2 \pm 0.3	17.5 \pm 0.2	2.6 \pm 0.8	2.6 \pm 0.4	292 \pm 2.8
	Layered structure	33.1 \pm 0.2	28.0 \pm 0.7	1.4 \pm 0.5	1.4 \pm 0.5	330 \pm 1.7	280 \pm 3.4
	Hybrid structure	65.7 \pm 0.9	49.1 \pm 0.1	1.5 \pm 0.2	1.4 \pm 0.7	350 \pm 2.4	310 \pm 3.1
Wet	Reference (PF)	0.32 \pm 0.05	0.21 \pm 0.08	0.54 \pm 0.07	0.47 \pm 0.4	201 \pm 0.2	197 \pm 0.2
	Layered structure	0.73 \pm 0.06	0.56 \pm 0.04	0.27 \pm 0.08	0.28 \pm 0.4	324 \pm 0.9	289 \pm 0.7
	Hybrid structure	1.9 \pm 0.04	0.82 \pm 0.03	0.31 \pm 0.05	0.34 \pm 0.8	346 \pm 0.7	302 \pm 0.9

269 SD = spin direction, CD = cross direction

270
 271 **Pore-size distributions and water flux.** A broad distribution of pore sizes and a high
 272 pore volume were detected for the reference membrane (**Figure S6a**). The maximum
 273 pore volume was in the range of 55-150 nm, which indicates macropores (> 50 nm).
 274 After the introduction of MFC (10 g/m²), a decrease in the pore size distribution and
 275 volume was detected. A drastic shift of the pore diameter and volume from 150 nm to
 276 78 nm and 1 nm to 0.03 nm, respectively, was observed (**Figure S6b**). The maximum
 277 distribution of the pores in the layered FSCM was found in the range of mesopores (2-
 278 50 nm). In the case of the hybrid FSCM, a pore size distribution (1 nm to 65 nm)
 279 lower than the reference and layered composite membranes was present.¹⁴
 280 Due to the pores distribution range limitation, (<1 nm to 150 nm) of N₂ gas adsorption
 281 technique (BET), Hg-porosimetry (pore-range, 5 nm-1 mm) was carried out. The
 282 open pores in the reference membranes were in the range of 3 to 10.7 μ m, and the
 283 maximum pore volume was in the range of 4 to 7 μ m.¹⁵

284

285 At a pressure of 0.5-1.5 bars, the water flux of all membranes was increased with
 286 respect to applied pressure. The highest water flux was reported for the reference
 287 membrane, followed by layered and hybrid flat sheet structures. The water flux of the
 288 reference at 1.5 bar was 9625 L/m²h, which further decreased to 7000 L/m²h for the
 289 layered flat sheet membranes, and the lowest flux was recorded for the hybrid flat
 290 sheet structures (6750 L/m²h) (**Figure S6d**). A very thin infused layer of MFC (≈ 50
 291 μm) was produced during the processing of the flat sheet layered membrane. This
 292 infused layer does not have any drastic hindrance forces for the free water flow and
 293 no significant decrease in the water flux was recorded. Thus, an ultrahigh water flow
 294 through the layered flat-sheet membranes could be due to the nanochannels inside the
 295 assembled MFC network as reported by Ma et al. and others.^{16,35,36}

296
 297 **Membranes performance for pollutants removal.** All six cationic metal ions
 298 targeted in this study are listed in **Table 3**. A very low removal percentage (1 to 3%)
 299 and removal capacity in the range of 0.7-1.2 mg/g of all the metal ions was recorded
 300 using the reference membranes. The highest removal (98%) was obtained with the
 301 layered FSCM for the Mn²⁺ ions followed by Cd²⁺. The whole removal percentage
 302 was in the order: Mn²⁺ > Cd²⁺ > Mg²⁺ > Cr³⁺ > Fe²⁺/Fe³⁺ > Co²⁺ and the removal
 303 capacity in the order: Mg²⁺ > Mn²⁺ > Cd²⁺ > Fe²⁺/Fe³⁺ > Cr³⁺ > Co²⁺, indeed, the
 304 removal capacity is a quantitative analysis that depends on the initial concentration of
 305 the individual metal ions.^{1,37-39}

306 In the case of layered assembled MFC membranes, a low contact angle is recorded
 307 due to the low density of carboxylic functional groups, increasing the hydrophilic
 308 character of the surface, which improves the immobilization capacity of the charged
 309 pollutants compared to the hybrid membranes.^{11,12,39}

310

311 **Table 3:** Removal experiment of industrial effluent in cross-flow mode

312

Name of metal ions	C _o ($\mu\text{g/L}$)	C _t ($\mu\text{g/L}$)		Removal (%)		Removal capacity (mg/g)	
		LCM	HCM	LCM	HCM	LCM	HCM
Fe ²⁺ /Fe ³⁺	616	244 \pm 0.029	341 \pm 1.10	60	44	157	142
Mg ²⁺	5800	1070 \pm 0.13	3350 \pm 0.42	81	42	737	717
Cd ²⁺	5.77	0.292 \pm 0.05	0.757 \pm 0.12	94	86	194	201
Co ²⁺	1.03	0.533 \pm 0.12	0.864 \pm 0.20	48	16	59	51
Cr ³⁺	9.87	3.32 \pm 0.65	7.55 \pm 1.95	66	23	64	67
Mn ²⁺	342	4.95 \pm 1.50	8.97 \pm 0.80	98	97	223	201

313 LCM = Layered composite membrane, HCM = Hybrid composite membrane

314

315 It was found that, despite the low charge density (48.45 \pm 4 $\mu\text{mole/g}$) and surface ζ -
 316 potential (-38 \pm 2.2 mV) of MFC, both composite membranes had a high removal
 317 capacity of all the metal ions. This is also evident from the analysis of the simulations

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2
3 318 results that identified possible capture mechanisms in the two architectures from the
4 319 RDFs and the cellulosic matrix pores and channels. In the layered system, where a
5 320 narrow canal filled with solvent separates the fibers (periodic representations), the
6 321 solvated glucosyl chains maintained an ordered orientation, and their packing
7 322 arrangement was almost preserved. A mild swelling was caused by the inner
8 323 adsorption of a few water molecules and hydrogen bonds with the first water shell
9 324 (within 3.5 Å), which contained approximately 43% of the surrounding waters. The
10 325 carboxyl functional groups, which were randomly distributed on all four fiber sides,
11 326 could be involved in interchain interactions, but most of the time, they were
12 327 deprotonated (80%) and pointed towards the solvent. This favored the capture of the
13 328 metal cations, as suggested by the trends displayed in **Figure S7**.
14 329

15 330 The presence of relatively sharp peaks at short distances in all the X-O(WAT) RDFs
16 331 suggests that all the ions were surrounded by water and could be found in solution or
17 332 close to the surface, still coordinated with a few water molecules. The Cr ions were
18 333 located preferentially in the middle of the channel or close (within 3.5 Å) to the
19 334 cellulose hydroxyl (12%) but far from the carboxyl oxygens that were, instead, the
20 335 target of the other two ions types, namely Fe and Mg. Indeed, 47% of the Fe ions
21 336 were connected to the carboxyl chains, as indicated by the two peaks at short Fe-
22 337 O(COO⁻) distances (2.1 and 3.0 Å). These peaks evidence the presence of
23 338 Fe₂O₃•3H₂O species that is further confirmed by the sharp peak centered at about 3 Å
24 339 in the Fe-Fe RDF profile displayed in **Figure S8**. On the contrary, only 7% of the Fe
25 340 ions interacted with the other oxygens of the fibers. Mg ions were also connected to
26 341 the carboxyl groups (20%) but located farther from the other cellulose oxygens (2%
27 342 within 3.5 Å). Furthermore, all the metal ions remained far from each other (at
28 343 separations greater than 5.5 Å).

29 344 The scenario is entirely different in the hybrid system. There, the ordering of the
30 345 chains was partially disrupted, and the carboxyl groups were randomly distributed
31 346 inside the cellulose matrix. The deprotonation of these moieties was reduced (60%),
32 347 and the cellulose water content increased in relation to the other system (92% of the
33 348 water molecules, instead of 80%, were found within 3.5 Å of the cellulose atoms).
34 349 The matrix showed a highly porous structure with big pockets, tunnels, and cavities
35 350 that could host water and ions. Depending on the local character (that is on the group
36 351 forming these areas), metal ions could remain entrapped, indirectly interact with other
37 352 metal ions, and hardly be released by the membrane. Possible interaction schemes and
38 353 pores structures were obtained by examining the RDF profiles of **Figures 3a-c** and
39 354 the membrane sections shown in **Figures 3d,e** and **S9**.
40 355

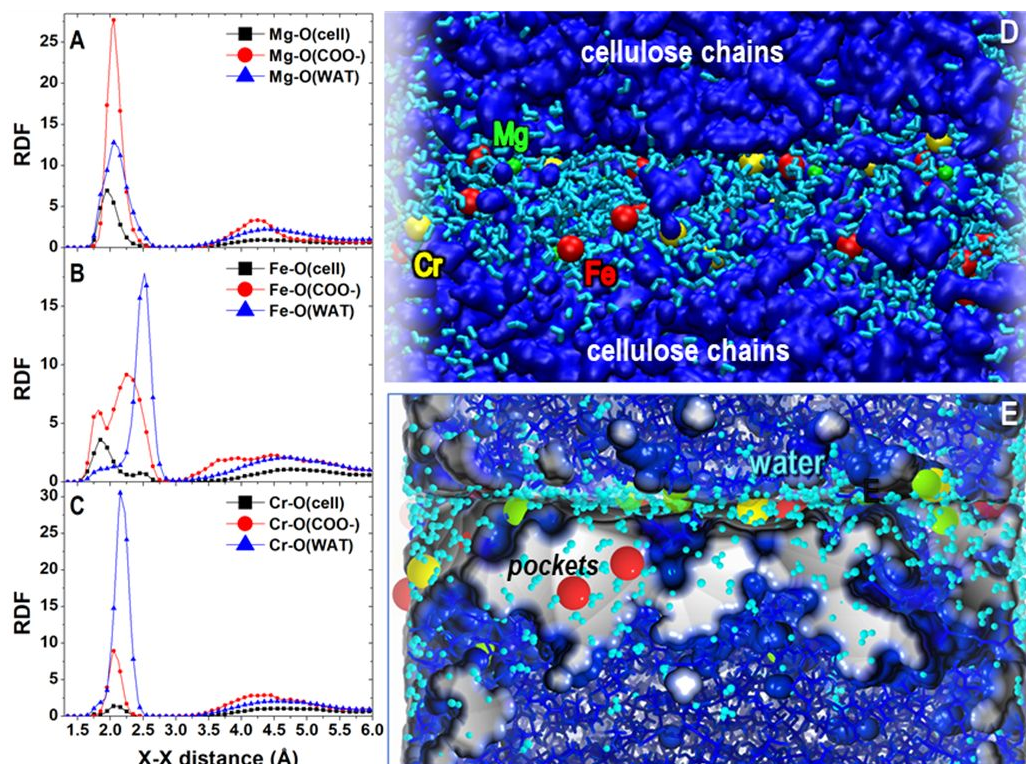


Figure 3. A, B, C) Radial distribution functions (RDFs), obtained from the final portions of the MD trajectories of the hybrid membrane model, between the metal ions and the cellulose oxygens not including the carboxyl ones [O(cell)], the carboxyl oxygens [O(COO⁻)] and water oxygens [O(WAT)]. D, E) Snapshot extracted from the final stage of the MD simulations. This magnification represents a section of the simulation box (parallel to the XZ plane) where pockets filled with water and ions are highlighted (solid blue-grey spheres) in E. In D, the cellulose chains are rendered through a solid blue solvent accessible surface, whereas blue sticks are used in E; the ions are depicted as red (Fe), yellow (Cr), and green (Mg) spheres; water molecules are cyan sticks. D) VMD visualization of a XZ section of the membrane and its corresponding CAVER representation with small and big pockets (E). Other perspective views are shown in **Figure S9** of the SI.

The sharp and broad red peaks at short distances in all the X-O(COO⁻) RDFs suggest that all the ions could directly interact with the carboxyl oxygens and sit at closer distances in a range of 1.8 - 2.2 Å. This indicates, again, given the two peaks in the Fe-O(COO⁻) and Fe-O(cell) RDF plots and in the Fe-Fe distance profile of Figure SM5, the presence of Fe₂O₃ species. The percentage population of the ions-cellulose connections in this hybrid organization of the chains is more balanced than in the layered model, being 41%, 45%, and 14% for Fe, Mg, and Cr, respectively, but in line with the previous trend of Cr ions. In fact, interactions between Cr and the cellulose oxygen atoms are weak, probably because of the competitive interactions with the other species. Only 28% of the Cr ions were located within 3.5 Å of the cellulose hydroxyls, whereas Fe and Mg had stronger interactions as confirmed by their percentage populations, namely 75% and 78% for Fe and Mg, respectively. Water molecules always surrounded the ions that could also be placed close to each other due to relatively strong immobilization and entrapment in narrow regions, as is evident in the RDF plots shown in **Figure S9** and in the membrane sections shown in **Figures 3e,f**.

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4 385 From an experimental point of view, it could be hypothesized that a combination of
5 386 adsorption, aggregation into bigger nanoparticles, and subsequent size-exclusion
6 387 could be the separation mechanism of metal ions from industrial effluent (**Figure**
7 388 **S10**). It was reported earlier that functional membranes prepared using cellulose
8 389 nanofibers with vacuum filtration, having an average pore diameter of 194 Å and a
9 390 few active groups on the surface, adopt a similar mechanism for removing the metal
10 391 ions.^{15,40,41}

11 392 The design of flat sheet composite membranes is also crucial. During the production
12 393 of the layered composite membranes, we sprayed MFCs on top of the pine base layer,
13 394 to tune both the pore size and structure of this region. We obtained a film that could
14 395 be easily seen by inspection of the SEM analysis (**Figure 2ci and 2cii**). This
15 396 modulated self-assembled architecture is essentially a sieve with finely arranged
16 397 narrow channels that could be controlled through the regulation of the top layer.⁴²⁻⁴⁴
17 398 This is very effective for a fast immobilization of a large number of metal ions.

18 399 The removal capacity of metal ions was further compared with
19 400 cellulose/nanocellulose and its derivatives, as reported in the literature. In the case of
20 401 ferric ions (Fe^{3+}), Q_{max} was 115¹ and 19 mg/g⁴⁵ for functionalized nanocellulose and
21 402 cellulose, respectively, and both values are lower in relation to those found in the
22 403 current study, which are 157 and 142 mg/g of removal capacity for the layered and
23 404 hybrid MFC assembled composite membranes, respectively. A high removal capacity
24 405 (335 mg/g) for Cd^{2+} was reported by Yu et al. 2013⁴⁶ using modified cellulose
25 406 (carboxylated cellulose). In another report, polymer grafting was performed to attach
26 407 amino groups on the surface of MFC, and surprisingly a low removal capacity (179
27 408 mg/g) was calculated.³⁸ Here, Cd^{2+} removal capacity was 201 mg/g of the used hybrid
28 409 composite membranes. In an article³⁷ TEMPO-oxidized functionalized cellulose
29 410 nanofibers used for the adsorption of Cr(III) at pH of 6.2 - 6.5, showed an adsorption
30 411 capacity of 58 mg/g, which is lower than the one measured here.³⁷ It might be
31 412 interesting to note that only the 10th pass of the industrial effluent was performed
32 413 through composite membranes. Thus the reported values are not for the saturation
33 414 limit. In parallel, all values reported in the literature denote the saturation limit (Q_{max}
34 415 values).

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36 417 **Separation of dyes impurities in cross-flow mode.** The 80% removal of IV H dye
37 418 was recorded using the layered FSCM, as shown in **Table S3**. The removal
38 419 percentage of IV H was further increased when a hybrid flat sheet membrane was
39 420 used, and reached 82%. A significant increase in percentage removal from 71% to
40 421 83% of IB RL, with respect to the layer and hybrid FSCM, was recorded, (**Table S3**,
41 422 **Figure 4**). In a previous study², the highest removal of 88 to 98% was found for
42 423 Victoria Blue 2B It is worth mentioning that bulk adsorption and ultrafast removal in
43 424 a dynamic mode made this approach more suitable and adequate for the industrial-
44 425 scale setup.

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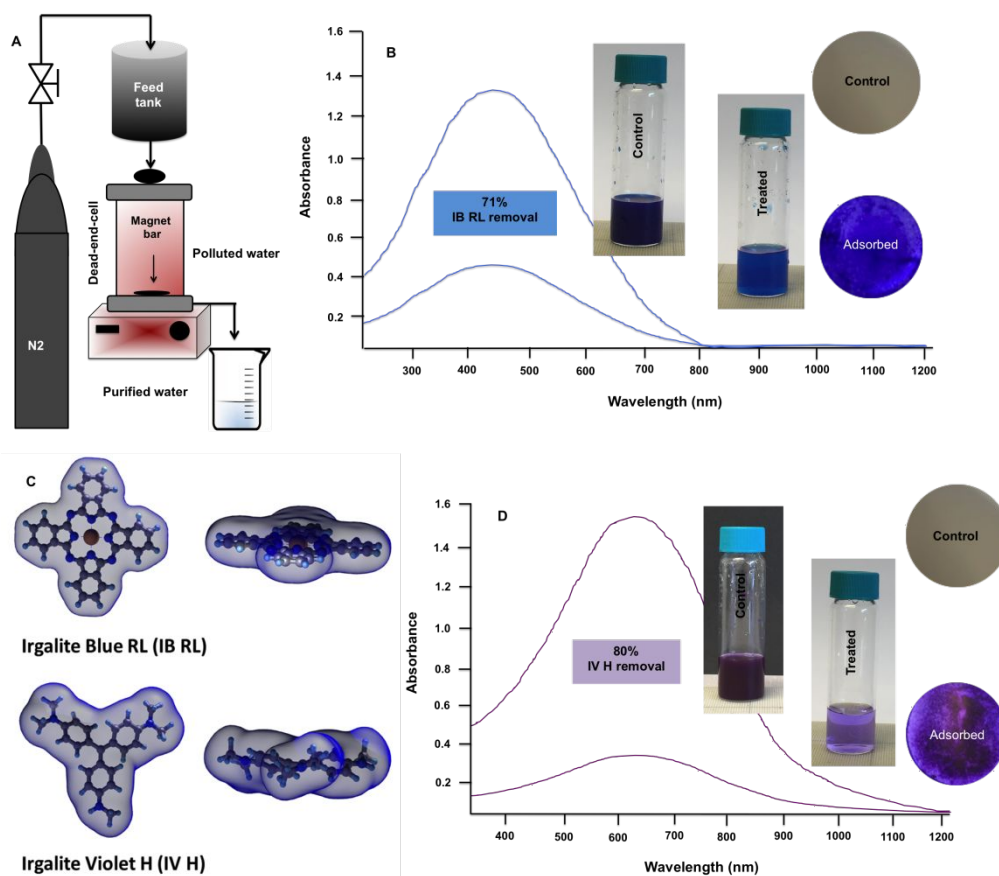
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 428 **Figure 4.** Removal experiment of dyes using the produced flat sheet composite membranes in cross-
 429 flow mode (A). The spectrum of Irgalite Blue RL was recorded at 449 nm (B). Irgalite Violet H visible
 430 spectrum is shown in (D), the spectrum was captured at a wavelength of 652 nm (λ_{\max}). The removal
 431 percentage was calculated as reported in equation (ii). A decrease in color intensity after separation can
 432 be easily seen. Furthermore, a change in color after filtration of the dyes solution confirmed the
 433 adsorption of the dye molecules on the surface of the composite membranes. Finally, optimized
 434 molecular structures of the two dyes (balls and sticks models) are shown (C).
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436 The effect of the charge and hydrodynamic/hydrated radius of the dyes on the
 437 retention of the surface of the membranes or inside their pockets and tunnels could be
 438 evaluated considering long-distance interactions, local character of the nanocellulose
 439 networks, and specific assembly of the fibers. The negatively charged functional
 440 groups of the chains imparted to the whole texture a negatively charged nature and
 441 thus the ability to attract positively charged ions. The intensity of this driving force
 442 was mitigated by the random distribution of the head groups on the fiber surfaces,
 443 their local density, and the presence of other moieties that could reduce their action
 444 through intramolecular hydrogen bonds. Indeed, after attraction and adsorption on the
 445 surface of the fibers, the dyes could remain entrapped in local pockets or channels
 446 inside the network and be kept there by the concerted action of the local moieties,
 447 namely carboxyl, hydroxyl, and epoxy groups present in the cellulose chains. It might
 448 be speculated that high retention of the dyes is obtained by favorable cooperative
 449 interactions, including charge neutralization and hydrophobic interactions of their
 450 rings with the hydrophobic portion of the cellulose chains. It was also observed that

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3 451 the selected dyes, which contain several conjugated rings, are quite rigid and have the
4 452 tendency to form molecular aggregates where the molecules can adopt stacked and T-
5 453 shape arrangements. This determined an increase in the hydrated radius and thus
6 454 enhanced retention.

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8 455 The adsorption of charged pollutants via available functional groups has been
9 456 reported extensively in the literature,^{42,47-50} and a similar phenomenon (**Figure S10**) is
10 457 also responsible for the removal mechanism of metal ions and dyes, whereas size-
11 458 exclusion becomes dominant afterward.

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15 460 **OUTLINE**

16 461 We have reported a fully water-based system for the up-scaling of MFC FSCMs (0.2
17 462 × 1 m). A Dynamic sheet former, a unique membrane processing device, is used to
18 463 produce two assembled architectures with a controlled congregation of MFC within a
19 464 long pine fibrous network (hybrid) and on top of it (layered). The assembly of MFC
20 465 has a direct influence on the final properties of membranes, such as ultrahigh water
21 466 permeability and open fibrous networks (layered membranes). Pilot-scale processing
22 467 of the membranes imparted extraordinary properties, like the orientation of fibers in
23 468 the spin direction of the machine (high tensile strength in spin direction), controlled
24 469 infusion of MFC within lone pine fibrous based layer, uniform pore-size structures,
25 470 and distribution, and tunable surface properties, which could be challenging to
26 471 achieve using a lab-based vacuum-filtration approach.¹¹ The up-scaled membranes
27 472 were used for the adsorption of dyes and metal ions from model and industrial water.
28 473 Both membranes showed effective removal of both the targeted metal ions and the
29 474 positively charged dyes. The available -OH⁻ and -COO⁻ functional groups on the
30 475 membrane's surface were responsible for the binding of metal ions. In the case of the
31 476 layered type, the ultrafast adsorption followed by the entrapment of the metal ions in
32 477 locations nearby caused the formation of metal clusters, which narrowed the channel
33 478 thus increasing the percentage removal.

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39 479 It might be interesting to use this proposed fully water-based system for the
40 480 continuous production of membranes for real module design. Large volume filtration
41 481 of industrial effluent contaminated with various types of pollutants and study on the
42 482 selectivity of pollutants towards grafted functional groups could be the future aim.

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46 484 **AUTHORS' CONTRIBUTIONS**

47 485 All work was carried out under the supervision of ZK. ZK carried out most of
48 486 experiments and analyzed, summarized and explained all the obtained results in the
49 487 article. DG performed flux measurement and pore-size distribution experiments, and
50 488 also contributing in writing the article. AS review the article. APM improved the
51 489 manuscript respect to journal standard. SM carried out all computational studies. All
52 490 authors read and approved the final manuscript.

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496 mechanical properties measurements, respectively. SM is grateful to the CINECA
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503 CONFLICT OF INTEREST

504 No conflict of interest has been reported.

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